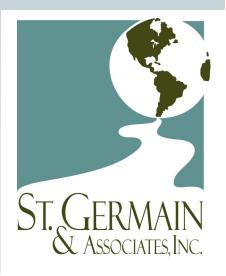
Ground Water Extraction, Surface Water Recharge, and the New DEP In-Stream Flow Rule: Rangeley Water District Case Study

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## Introduction

- The Rangeley Water District (RWD) taps a remote aquifer for its water supply in Dallas Plantation
- The well is close to the South Branch of the Dead River
- The LURC permit for the well restricts withdrawal based on the flow rate of the South Branch
- A new DEP regulation restricts direct or indirect withdrawal from Maine rivers

## Introduction

- Is the river-flow based restriction on pumping reasonable?
- What is the actual influence of the well on the stream (and vice versa)?
- How does the current flow-based restriction compare to the new DEP rules?
- Can the RWD increase its pumping rate without harming the river ecosystem?

## **Presentation Outline**

- 1. <u>Background</u> on the RWD and its supply
- 2. Regional Hydrogeology of the aquifer
- 3. <u>Local Hydrogeology</u> of the aquifer and well
- 4. New DEP Ch. 587 In-Stream Flow Rule
- 5. <u>River to Well Recharge estimates</u>
- 6. <u>Resolution of RWD supply needs and</u> DEP flow rules

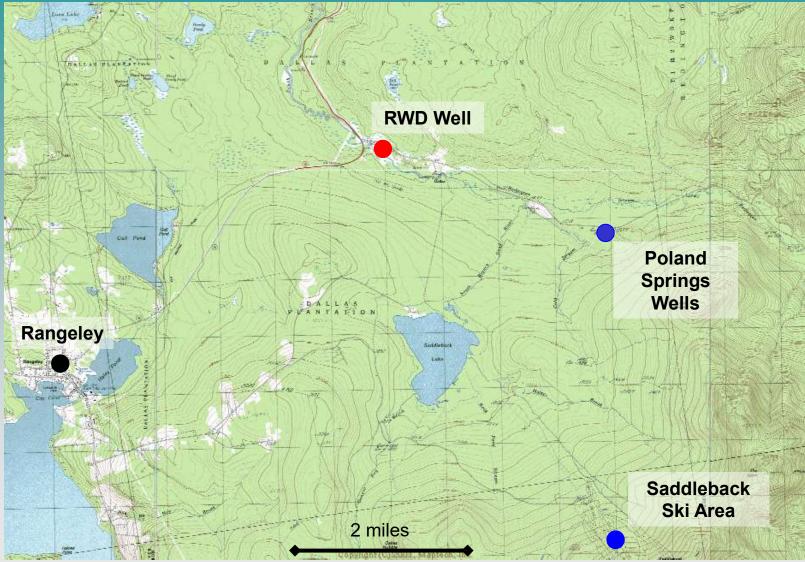
## 1. Background

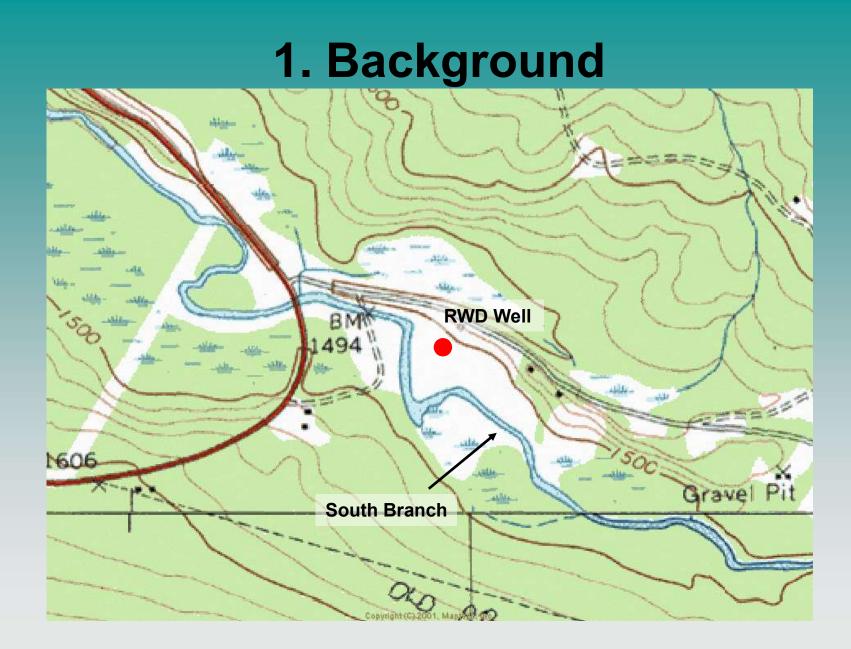
#### **Rangeley Water District**

- Serves 965 in Rangeley area from a well drilled in 1995. Well is in Dallas Plt. northeast of town.
- When pumping, rate is 250 gpm for about 80,000 gallons per day (~6 hrs/night or 60 gpm annual average).
- Well located within 200 feet of the South Branch of the Dead River (South Branch).
- LURC permits restricts withdrawal to 0.5 cfs (225 gpm) if stream flow <17 cfs (based on USFWS aquatic baseflow (ABF) of 0.5 cfsm)

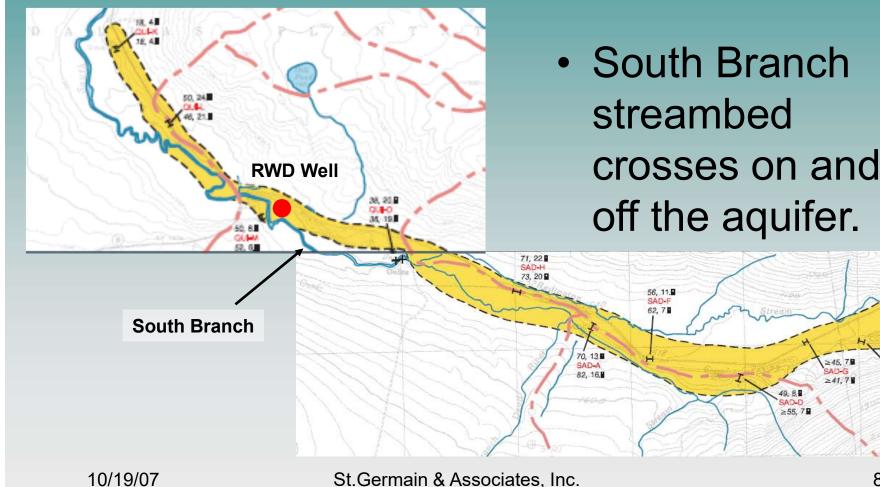
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## 1. Background





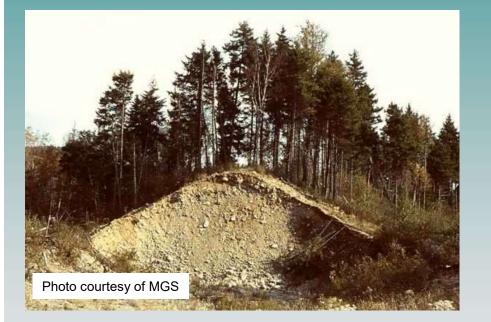
2. Regional Hydrogeology South Branch valley filled with 50 to 70 feet of sand and gravel. Narrow aquifer.



≥41.7

SAD-D ≥55, 7. ≥60, 19 ₽

2. Regional Hydrogeology
Part of valley fill sand and gravel consists of an esker.

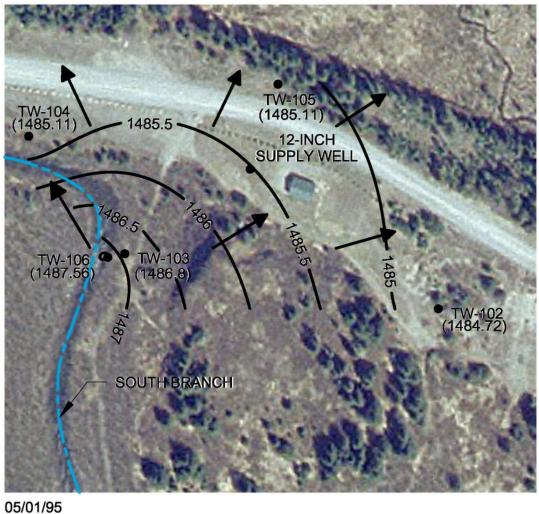


 Esker was the target of B.
 Caswell when he sited the well.

# Poland Spring wells can yield 400 gpm, esker very productive.

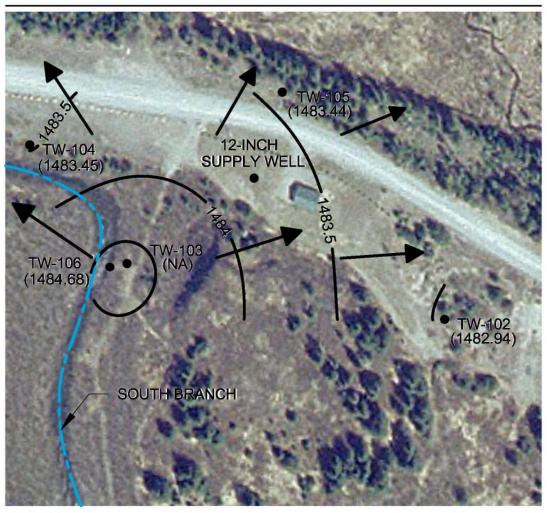
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- Ground water elevation measurements were collected from monitoring wells (Oct, Nov, Dec, Apr, May)
- Stream flow measurements collected near well (by Poland Springs)
- 5 ground water contour maps prepared



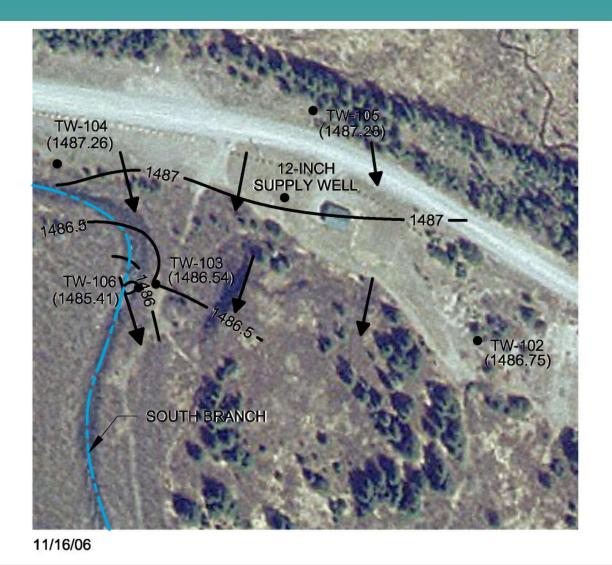
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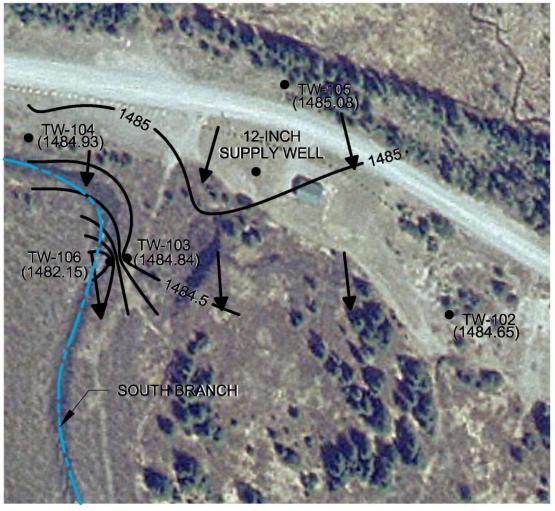


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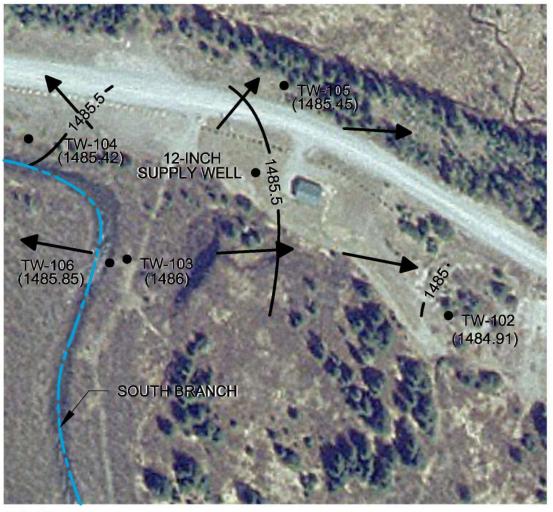


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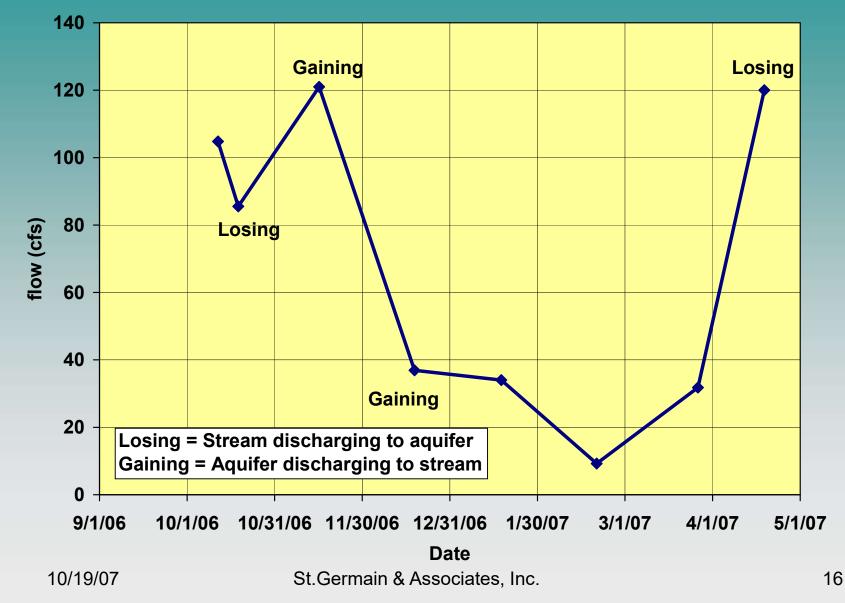
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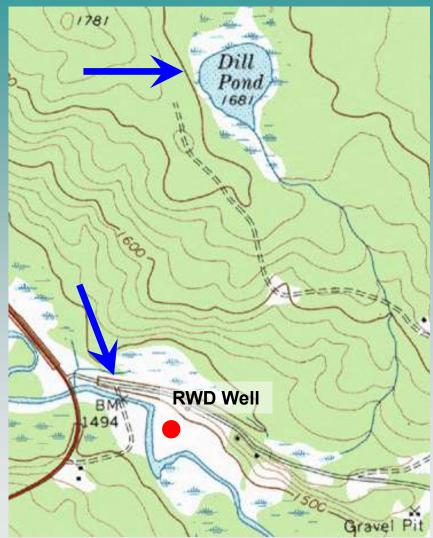
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#### **Observations**

- Stream and aquifer "flip-flop" recharge roles frequently
- No consistent relationship between stream flow and recharge
- Other factors probably play a role:
  - Frozen ground inhibiting direct recharge
  - Local discharge from nearby pond (see map)
  - Damming effect of bridge (see map)



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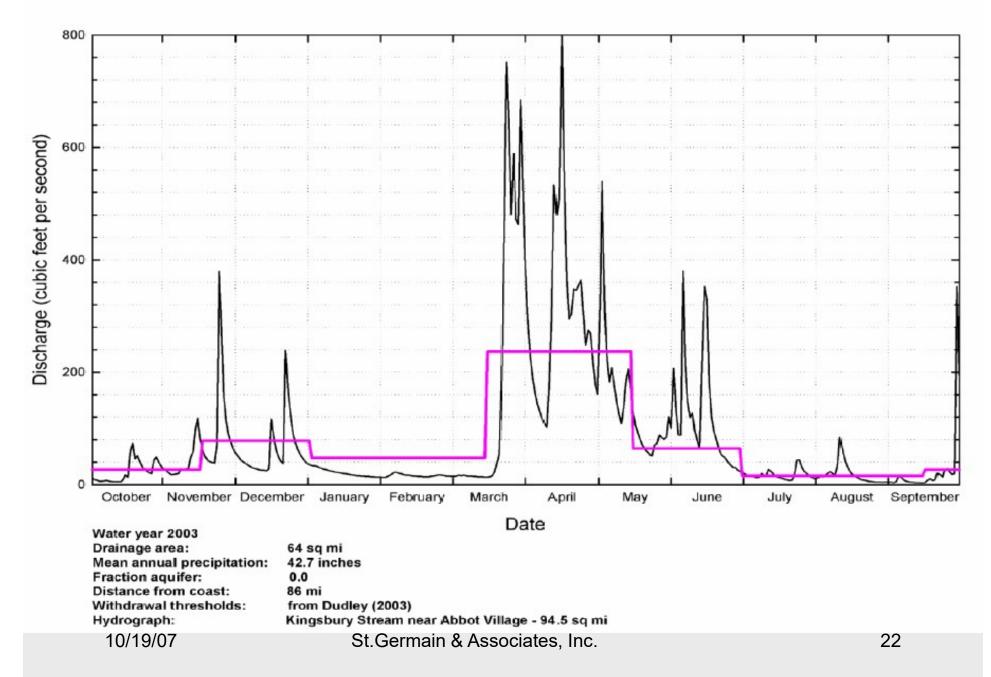
- "Establishes river and stream flows and lake and pond water levels to protect natural aquatic life and other designated uses in Maine's waters"
- Actually puts aquatic life ahead of other uses with the exception of public water supplies
- Effective August 2007
- Focus here is on stream flow

- Rule's ideal goal is to prohibit withdrawals when flow is below seasonal median
- Contrast with USFWS ABF of 0.5 cfsm
- Rules separate Class AA, A, and B/C streams; South Branch Class A stream
- <u>Regulated withdrawal from Class AA and A</u> includes nearby wells
- Seasonal median determined from 10 yrs data from site or similar watershed or...
- Dudley USGS regression calculations based on water shed characteristics

#### **In-Stream Flow Standards**

Season	Begin	End	Median Standard	
Winter	1-Jan	15-Mar	February	
Spring	16-Mar	15-May	April	
Early Summer	16-May	30-Jun	June	
<u>Summer</u>	<u>1-Jul</u>	<u>15-Sep</u>	<u>August</u>	
Fall	16-Sep	15-Nov	October	
Early Winter	16-Nov	31-Dec	December	

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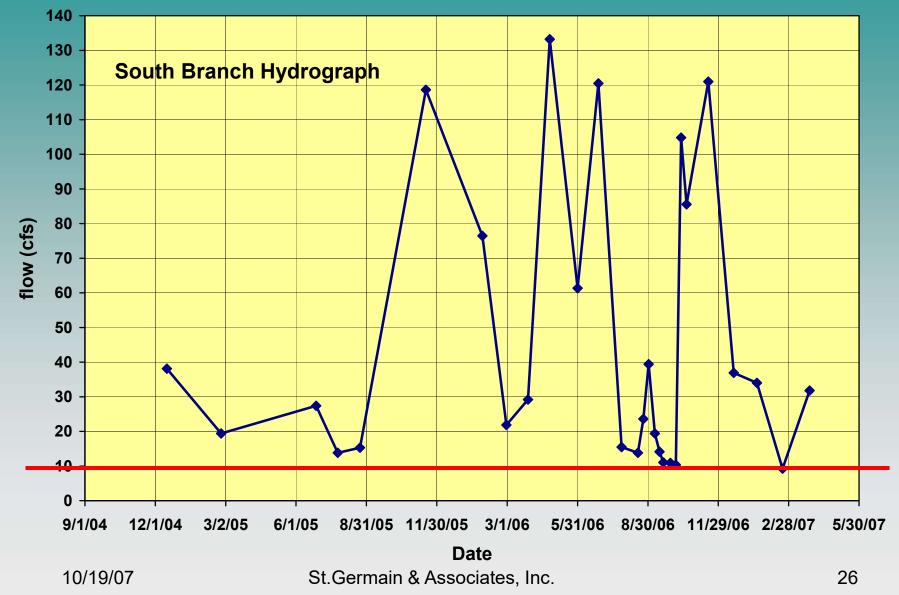
Several ways to get DEP to approve alternatives:

- Water Flow Plan
- Withdrawal Certificate for Public Supplies
- Exceptions for droughts
- Existing permits from LURC or for hydropower stay in effect
- DEP also agreed not to require Public Supplies to meet standards until 5 years after DEP asks.

- RWD wanted to remove LURC permit limitations on withdrawal (0.5 ABF outdated) but had to consider new DEP Rule
- Low pumping rate suggested well had little influence on stream
- Ground water contour maps did not show consistent pattern between stream flow and ground water flow
- Not a simple "well feeding off stream" scenario

Streamflow statistics using Dudley methods

$Q = 1.151 (A)^{0.991} 10^{0.023 pptW}$								
A (acres)*	A (sq.mi.)	pptW**	Q (cfs)	Q actual***				
21,993	34.36	8.4	59.8	45				
$Q = 0.239 (A)^{1.006} 10^{0.057 \text{pptW}}$								
			Q (cfs)	Q actual***				
21,993	34.36	8.4	25.3	28				
$Q = 0.152 (A)^{1.120} 10^{1.31SG}$								
			Q (cfs)	Q actual***				
21,993	34.36	0.05	9.4	NA				
	A (acres)* 21,993 Q = 0.23 A (acres)* 21,993 Q = 0.14 A (acres)*	A (acres)*A (sq.mi.)21,99334.36Q = $0.239 (A)^{1.00}$ A (acres)*A (sq.mi.)21,99334.36Q = $0.152 (A)^{1.12}$ A (acres)*A (sq.mi.)	A (acres)*A (sq.mi.)pptW**21,99334.368.4Q = 0.239 (A) $1.006$ 10 $0.057$ fA (acres)*A (sq.mi.)pptW (in.)**21,99334.368.4Q = 0.152 (A) $1.120$ 10 $1.315$ fA (acres)*A (sq.mi.)SG*	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$				



- Streamflow capture analysis
- Jenkins, 1970 (who based his math on Theis, Hantush, etc.) Available reference is Peters, 1987 (USGS WRIR 86-4199)
- Uses nomographs and calculations based t, Q, T, S, a. Basic assumptions:
  - T, Q constant
  - Isotropic, homogeneous aquifer (no delay)
  - Fully penetrating, straight stream

	tp or						
S	tp + ti	V	q	q	V	V	V
	d	gal	ft3/d	cfs	ft3	gal	% of V
0.25	0.23	82,800	14,920	0.17	1,439	10,764	13.0%
0.25	0.5	0	5,775	0.07	4,813	36,000	43.5%
0.25	0.75	0	3,369	0.04	5,535	41,400	50.0%
0.25	1	0	2,406	0.03	7,219	54,000	65.2%
0.1	0.23	82,800	26,470	0.31	3,653	27,324	33.0%
0.1	0.5	0	4,813	0.06	4,813	36,000	43.5%
0.1	0.75	0	1,925	0.02	5,775	43,200	52.2%
0.1	1	0	963	0.01	6,738	50,400	60.9%
0.25	1	360,000	28,877	0.33	19,732	147,599	41.0%
0.1	1	360,000	36,096	0.42	28,877	215,998	60.0%

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- Calculations show:
- After one night of pumping, contribution from stream had reached about 0.2 cfs, but rate drops quickly when pumping stops
- About 60% of water from stream over entire pumping cycle, but withdrawal rate (v) remains low
- Peak recharge rate from stream equals about 3% of predicted August median stream flow (9 cfs)

- If pumping 24 hrs at 250 gpm (rather than 6 hr/night), v increases to 0.4 cfs or about 4% of August median
- Even if all pumped water came from stream, it would only equal about 6% of August median stream flow
- Model is conservative because:
  - Stream is fully penetrating
  - No recharge to aquifer
  - Does not consider variations in stream flow

## 6. Summary

- Estimated August median flow is about 9 cfs, less than in permit (based on 0.5 cfsm ABF)
- Original LURC restriction on flow (0.5 cfs withdrawal max if stream flow is <17 cfs) overly conservative:
  - August median is much lower than ABF suggests (9 vs 17 cfs)
  - Ground water flow and stream flow do not have close relationship
  - Pumping predicted to use less than 5% of stream flow under August median conditions

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## 6. Summary

- Application to alter LURC permit conditions
   submitted last month
- Requests pumping at 250 gpm up to 24 hrs per day
- With that said, DEP says they are not really interested in flow rate calculations
- Will base decision on visual inspection of stream ecosystem such as wetted surface (?)
- One of the first applications of new rule...